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TITLE: Circularly-Polarized-Wave Patch  
Antenna Which Can Be Used in a  
Wide Frequency Band

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CIRCULARLY-POLARIZED-WAVE PATCH ANTENNA WHICH CAN BE USED IN  
A WIDE FREQUENCY BAND

BACKGROUND OF THE INVENTION

5 1. Field of the Invention

The present invention relates to a circularly-polarized-wave patch antenna. In particular, the present invention relates to a configuration of a feeder circuit thereof.

2. Description of the Related Art

10 In recent years, patch antennas, which are compact and thin circularly-polarized-wave antenna, have been becoming widespread. In this type of patch antenna, a main body of the antenna is formed by providing a patch electrode and a ground electrode on both principal surfaces of a dielectric  
15 substrate. In this configuration, a predetermined high-frequency signal is supplied to a feeding point of the patch electrode so as to excite two orthogonal modes whose phases are different by  $90^\circ$ . Accordingly, a circularly polarized radio wave is radiated.

20 A single-point feeding method or a two-point feeding method can be adopted in a circularly-polarized-wave patch antenna. In general, a single-point feeding method is adopted because of its simple configuration. In the circularly-polarized-wave patch antenna using a single-point  
25 feeding method, a degenerate isolation element (perturbation element), such as a notch, is loaded on the patch electrode, and only one feeding point is provided on the patch electrode. One end of a feeding pin, which extends through the

dielectric substrate, is connected to the feeding point, and the other end of the feeding pin is connected to a feeder line, such as a coaxial cable. In the patch antenna of a single-point feeding type configured in the above-described manner, by adequately adjusting an area ratio of the patch electrode to the degenerate isolation element and the position of the feeding point, a phase difference of  $90^\circ$  can be generated between two orthogonal modes, having an equal amplitude and a different resonance length. Accordingly, the patch antenna can be operated as a circularly-polarized-wave antenna.

However, in the circularly-polarized-wave patch antenna using the single-point feeding method, a band of resonance-frequency for generating a phase difference of  $90^\circ$  between the two orthogonal modes is narrow. Therefore, a bandwidth in which a satisfactory axial ratio characteristic required for the circularly-polarized-wave antenna can be obtained, that is, a bandwidth in which the axial ratio of an elliptically polarized wave is under a permissible value, is quite narrow. Accordingly, a favorable axial ratio characteristic cannot be obtained in a wide band.

On the other hand, in a patch antenna using the two-point feeding method, a patch electrode is circular or square-shaped and a degenerate isolation element is not loaded thereon. Two signals whose phases are different by  $90^\circ$  are supplied to two feeding points provided on the patch electrode. A  $90^\circ$ -phase-difference circuit is provided between the input port of a feeder circuit and the patch

antenna. With this configuration, a phase of one signal supplied to one of the feeding points of the patch antenna is always delayed by  $90^\circ$  with respect to a phase of another signal supplied to the other feeding point. Accordingly, the  
5 two orthogonal modes of the patch electrode are excited with a phase difference of  $90^\circ$ , and thus the patch antenna can be operated as a circularly-polarized-wave antenna. In the patch antenna using the two-point feeding method, signals whose phases are different from each other by  $90^\circ$  are  
10 supplied to the two feeding points so as to excite the two orthogonal modes. As a result, a favorable axial ratio characteristic can be obtained over a wide frequency band.

As described above, a favorable axial ratio characteristic can be obtained in a wide band by adopting a  
15 circularly-polarized-wave patch antenna including two feeding points. However, in a known patch antenna of a two-point feeding type, it is not easy to supply electric power to the two feeding points of the patch electrode over a wide frequency band without reflection. Further, since reflection  
20 of signal waves is more likely to increase due to the limited frequency band of the patch antenna itself, a favorable reflection characteristic cannot be obtained in a wide band. This is because isolation of a pair of transmission lines of the  $90^\circ$ -phase-difference circuit connected to the patch  
25 electrode is difficult to ensure.

#### SUMMARY OF THE INVENTION

The present invention has been made in view of the state

of the known art, and it is an object of the present invention to provide a circularly-polarized-wave patch antenna which can be used in a wide frequency band by realizing a favorable axial ratio characteristic and  
5 reflection characteristic in a wide band.

In order to achieve the above-described object, a patch antenna of the present invention includes a main body having a dielectric substrate in which a patch electrode is provided on one principal surface thereof and a ground electrode is  
10 provided on another principal surface thereof, two feeding points being provided in the patch electrode; a  $90^\circ$ -phase-difference circuit for generating a phase difference of  $90^\circ$  between high-frequency signals supplied to the two feeding points through a pair of output terminals connected to the  
15 feeding points; and a Wilkinson distribution circuit including a pair of output terminals connected to the  $90^\circ$ -phase-difference circuit. An input terminal of the Wilkinson distribution circuit is connected to a feeder line so that the main body radiates a circularly polarized radio wave.

20 By connecting the  $90^\circ$ -phase-difference circuit to the two feeding points of the patch electrode, a favorable axial ratio characteristic can be obtained in a wide band in the patch antenna. Further, the Wilkinson distribution circuit is provided between the  $90^\circ$ -phase-difference circuit and the  
25 coaxial cable serving as a feeder line. Therefore, even if reflection is occurred at the patch electrode, this reflection is absorbed by a resistor of the Wilkinson distribution circuit through the  $90^\circ$ -phase-difference circuit,

so that the electric power supplied from the feeder line can be evenly distributed to the feeding points of the patch electrode in a wide frequency band without reflection. As a result, reflection of a signal wave can be significantly  
5 reduced, and thus a favorable reflection characteristic can be obtained in a wider band. Accordingly, a circularly-polarized-wave patch antenna, in which an axial ratio characteristic and a reflection characteristic are favorable over a wide frequency band, can be obtained.

10       The Wilkinson distribution circuit includes a junction; two parallel-connected line conductors connected to the junction, each line conductor having an electric length of  $\lambda/4$  and a characteristic impedance of  $\sqrt{2 \times Z_1 \times Z_2}$ , wherein  $Z_1$  is an input impedance of the Wilkinson distribution circuit,  
15  $Z_2$  is an input impedance of the main body, and  $\lambda$  is a wavelength of the high-frequency signal on a transmission line; and a resistor whose both ends are connected between the 90°-phase-difference circuit and the line conductors, the resistance of the resistor being  $2 \times Z_2$ . In general, since the  
20 characteristic impedance of the coaxial cable serving as a feeder line is about 50  $\Omega$ , the input impedance of the Wilkinson distribution circuit is 50  $\Omega$ , the characteristic impedance of each of the line conductors is about 70  $\Omega$ , and the resistance of the resistor is about 100  $\Omega$ .

25       In the patch antenna having such a feeder circuit, the 90°-phase-difference circuit and the Wilkinson distribution circuit are provided on a lower surface of a circuit board, which is fixed to a lower surface of the ground electrode of

the main body in a laminating manner, upper ends of two feeding pins which extend through the dielectric substrate and the circuit board are connected to the feeding points, and lower ends of the two feeding pins are connected to the output terminals of the 90°-phase-difference circuit. With this configuration, the main body and the circuit board are integrated, so that a compact patch antenna which can be used in a wide band can be preferably obtained. In this case, the dielectric substrate of the main body and the circuit board used for the feeder circuit may be included in a multilayer substrate. Also, instead of using the two feeding pins, two microstrip lines may be connected to the patch electrode for performing feeding. In this configuration, by providing the 90°-phase-difference circuit and the Wilkinson distribution circuit between the microstrip lines and the feeder line, the patch antenna can be used in a wider band.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a cross-sectional view of a patch antenna according to an embodiment of the present invention;

Fig. 2 is a bottom view of the patch antenna;

Fig. 3 shows the configuration of a feeder circuit of the patch antenna; and

Fig. 4 is a front view of the patch antenna.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

Hereinafter, an embodiment of the present invention will be described with reference to the above listed figures.

The patch antenna shown in the above listed figures, 1, 2, 3, and 4, includes a main body 1 having a dielectric substrate 2; a patch electrode 3 provided on an upper surface of the dielectric substrate 2; and a ground electrode 4 formed on an entire lower surface of the dielectric substrate 2. Further, a circuit board 5 is fixed to a lower surface of the ground electrode 4 of the main body 1 in a laminating manner. Also, a 90°-phase-difference circuit 6 and a Wilkinson distribution circuit 7 are provided on a lower surface of the circuit board 5.

Two feeding points P1 and P2 are provided in the patch electrode 3 of the main body 1. These feeding points P1 and P2 are defined by the upper ends of two feeding pins 8 and 9, the upper ends being soldered to predetermined positions of the patch electrode 3. As shown in Fig. 1, the feeding pins 8 and 9 extend through the dielectric substrate 2 and the circuit board 5. The lower ends of the feeding pins 8 and 9 are connected to different output terminals of the 90°-phase-difference circuit 6. In the embodiment, the dielectric substrate 2 is square-shaped, each edge thereof being about 28 mm, and the patch electrode 3 is also square-shaped, each edge thereof being about 16 mm, when viewed in a plan view.

As shown in Figs. 2 and 3, a pair of transmission lines 6a and 6b of the 90°-phase-difference circuit 6 are connected to a pair of output terminals of the Wilkinson distribution circuit 7, and an input terminal of the Wilkinson distribution circuit 7 is connected to an internal conductor of a coaxial cable 20. The Wilkinson distribution circuit 7



includes a junction 10 whose input side is connected to the coaxial cable 20, two line conductors 11 and 12 connected to an output side of the junction 10, and a resistor 13 for coupling the output sides of the line conductors 11 and 12.

5 Both ends of the resistor 13 are connected between the 90°-phase-difference circuit 6 and the line conductors 11 and 12. The two line conductors 11 and 12 are connected in parallel to each other. When the wavelength of a signal wave on the transmission line is  $\lambda$ , the electric length of each of the

10 line conductors 11 and 12 is set to  $\lambda/4$ . Also, when the input impedance of the Wilkinson distribution circuit 7 is  $Z_1$  and the input impedance of the main body 1 is  $Z_2$ , the characteristic impedance  $Z_3$  of each of the line conductors 11 and 12 is defined by the following equation:  $Z_3 = \sqrt{2 \times Z_1 \times Z_2}$ .

15 The resistance  $R$  of the resistor 13 is set to  $2 \times Z_2$ . For example, since the characteristic impedance of the coaxial cable 20 is 50  $\Omega$ , the input impedance  $Z_1$  of the Wilkinson distribution circuit 7 is 50  $\Omega$ . Accordingly, the characteristic impedance  $Z_3$  of each of the line conductors 11

20 and 12 is set to about 70  $\Omega$ , and the resistance  $R$  of the resistor 13 is set to 100  $\Omega$ .

The transmission line 6a of the 90°-phase-difference circuit 6 is provided with a line conductor 14 having a characteristic impedance of 50  $\Omega$  and an electric length of 0,

25 and the transmission line 6b is provided with a line conductor 15 having a characteristic impedance of 50  $\Omega$  and an electric length of 0 and a line conductor 16 having a characteristic impedance of 50  $\Omega$  and an electric length of

$\lambda/4$ . With this configuration, the phase of a signal supplied to the feeding point P2, which is connected to the transmission line 6b, is always delayed by  $90^\circ$  with respect to the phase of a signal supplied to the feeding point P1, which is connected to the transmission line 6a.

In the patch antenna configured in the above-described manner, two orthogonal modes of the patch electrode 3 are excited with the phase difference of  $90^\circ$  so as to radiate a circularly polarized radio wave. Since this patch antenna includes two feeding points, a desirable axial ratio characteristic can be obtained over a wide frequency band. Furthermore, in this patch antenna, the Wilkinson distribution circuit 7 is provided between the  $90^\circ$ -phase-difference circuit 6 and the coaxial cable 20. Therefore, even if reflection is occurred at the patch electrode 3, this reflection is absorbed by the resistor 13 of the Wilkinson distribution circuit 7 through the  $90^\circ$ -phase-difference circuit 6, so that the electric power supplied from the coaxial cable 20 is evenly distributed to the transmission lines 6a and 6b without reflection. Accordingly, reflection of a signal wave can be significantly reduced over a wide frequency band, and thus a favorable reflection characteristic can be obtained over a wide band. In this way, a favorable reflection characteristic as well as a favorable axial ratio characteristic can be obtained in a wider band, and thus the patch antenna according to the embodiment serves as a circularly-polarized-wave antenna which can cover radio waves over a wide frequency band.

Further, since the main body 1 and the circuit board 5 are integrated, a compact and thin patch antenna for a wide band can be obtained, which is highly practical. In the embodiment, the main body 1 and the circuit board 5 are bonded to each other so as to form the antenna. Alternatively, a multilayer substrate including the dielectric substrate 2 and the circuit board 5 may be used. Also, instead of using the two feeding pins 8 and 9, two microstrip lines (not shown) may be connected to the patch electrode 3 for performing feeding. In this configuration, by providing the  $90^\circ$ -phase-difference circuit 6 and the Wilkinson distribution circuit 7 between the microstrip lines and the coaxial cable serving as a feeder line, the patch antenna can be used in a wider band.

The present invention is realized in the above-describe manner, and has the following advantages.

According to the patch antenna of the present invention, a two-point feeding method is used, in which the  $90^\circ$ -phase-difference circuit is connected to the two feeding points of the patch electrode. With this configuration, a favorable axial ratio characteristic can be obtained in a wider band. Also, the Wilkinson distribution circuit is provided between the  $90^\circ$ -phase-difference circuit and the coaxial cable serving as a feeder line so as to improve an isolation characteristic and to obtain a favorable reflection characteristic in a wider band. Accordingly, a compact, thin, and highly practical circularly-polarized-wave antenna which can cover radio waves in a wide bandwidth can be obtained.